

Methanol Reactor. Hydrogenation of CO₂ to form CH₃OH on a Cu/ZnO/Al₂O₃ catalyst.

ORIGIN := 1

This catalyst converts methanol from CO₂ (not much from CO) and H₂, and it also catalyzes the formation of CO₂ from CO via the reversible water gas shift reaction.

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There are 8 chemical species. Assign ID numbers to names. $i := 1..8$ $R := 8.314$ J/mole-K

(CH₄ H₂O H₂ CO CO₂ O₂ N₂ CH₃OH) := (1 2 3 4 5 6 7 8)

stoichiometric coefficients

Reaction 2r: CO₂ + H₂ \longleftrightarrow CO + H₂O $v_{2r} := (0 \ 1 \ -1 \ 1 \ -1 \ 0 \ 0 \ 0)^T$

Reaction 5: CO₂ + 3 H₂ \longleftrightarrow CH₃OH + H₂O $v_5 := (0 \ 1 \ -3 \ 0 \ -1 \ 0 \ 0 \ 1)^T$

Kinetic model parameters from Vanden Bussche & Froment, J. Catalysis, 161, 1–10 (1996),

Table 2.

$K_{H_2}(T) := 0.499 \cdot \exp\left(\frac{17197}{R \cdot T}\right)$... sqrt(K_{H_2}) in Vanden Bussche & Froment

$K_{H_2O}(T) := 6.62 \cdot 10^{-11} \cdot \exp\left(\frac{124119}{R \cdot T}\right)$... K_{H_2O} in Vanden Bussche & Froment

$K_{H_2OH_2}(T) := 3453.38$... $K_{H_2O}/K_8/K_9/K_{H_2}$ in Vanden Bussche & Froment

$k_5(T) := 1.07 \cdot \exp\left(\frac{36696}{R \cdot T}\right)$... $K'_{5a} \cdot K'_2 \cdot K_3 \cdot K_4 \cdot K_{H_2}$ in Vanden Bussche & Froment, in mol/s/kg catalyst

$k_{2r}(T) := 1.22 \cdot 10^{10} \cdot \exp\left(\frac{-94765}{R \cdot T}\right)$... k'_1 in Vanden Bussche & Froment (note the sign)

Equilibrium constants

$K_{MeOH}(T) := 10^{\frac{3066}{T} - 10.592}$... K_1 in Vanden Bussche & Froment

$K_{RWGS}(T) := 10^{\frac{-2073}{T} + 2.029}$... $1/K_3$ in Vanden Bussche & Froment

Reaction rates

methanol synthesis (Reaction 5)

$$r_5(p, T) := k_5(T) \cdot p_{CO_2} \cdot p_{H_2} \cdot \frac{1 - \frac{1}{K_{MeOH}(T)} \cdot \frac{p_{CH_3OH} \cdot p_{H_2O}}{p_{CO_2} \cdot (p_{H_2})^3}}{\left(1 + K_{H_2OH_2}(T) \cdot \frac{p_{H_2O}}{p_{H_2}} + K_{H_2}(T) \cdot \sqrt{p_{H_2}} + K_{H_2O}(T) \cdot p_{H_2O}\right)^3}$$

reverse WGS (Reaction 2r)

$$r_{2r}(p, T) := k_{2r}(T) \cdot p_{CO_2} \cdot \frac{1 - \frac{1}{K_{RWGS}(T)} \cdot \frac{p_{CO} \cdot p_{H_2O}}{p_{CO_2} \cdot p_{H_2}}}{1 + K_{H_2OH_2}(T) \cdot \frac{p_{H_2O}}{p_{H_2}} + K_{H_2}(T) \cdot \sqrt{p_{H_2}} + K_{H_2O}(T) \cdot p_{H_2O}}$$

Isothermal Methanol Reactor. $T := 500$ K $P := 100$ bar

$m_{\text{cat}} := 1.64$ kg catalyst per basis = 1 mole of feed to methanol reactor \longrightarrow
need to scale up to the specified capacity later

$$dndt := v \cdot r = v_5 \cdot r_5 + v_{2r} \cdot r_{2r}$$

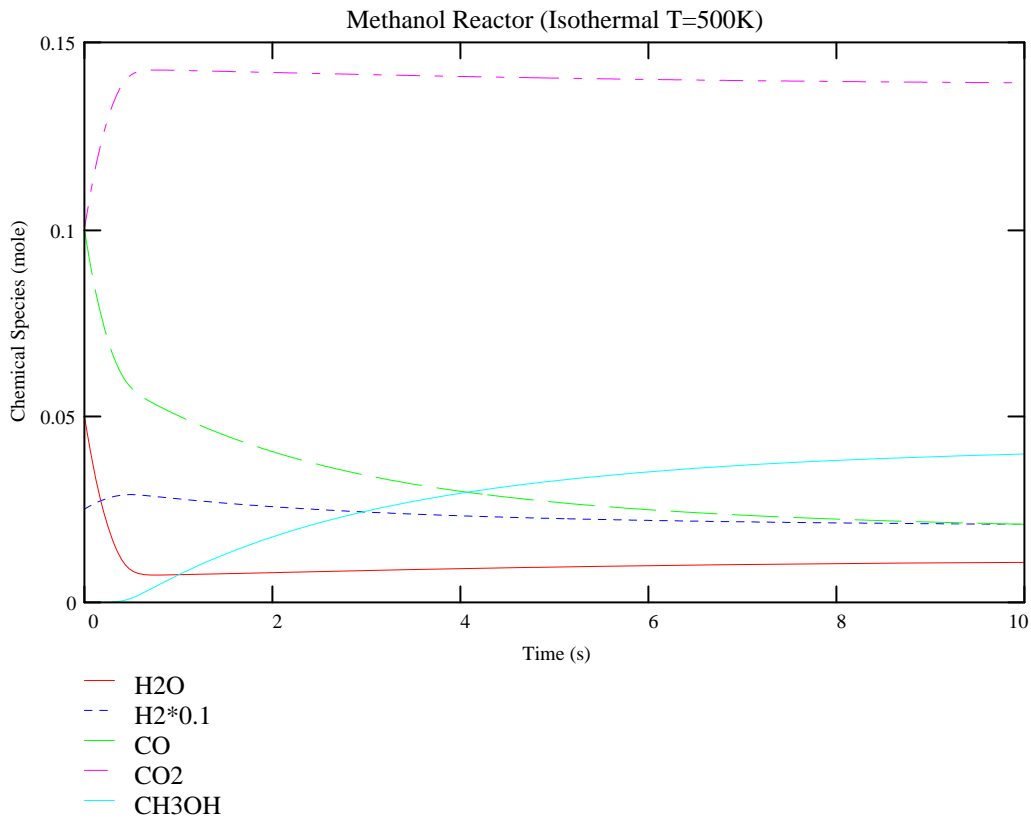
$$dndt(t, n) := m_{\text{cat}} \cdot v_5 \cdot r_5 \left(\frac{n}{\sum n}, P, T \right) + m_{\text{cat}} \cdot v_{2r} \cdot r_{2r} \left(\frac{n}{\sum n}, P, T \right)$$

I.C. $n_{\text{init}} := \begin{pmatrix} \text{CH}_4 & \text{H}_2\text{O} & \text{H}_2 & \text{CO} & \text{CO}_2 & \text{O}_2 & \text{N}_2 & \text{CH}_3\text{OH} \\ 0 & 0.05 & 0.25 & 0.1 & 0.1 & 0 & 0.5 & 0 \end{pmatrix}$ $n_{\text{init}} := \left(n_{\text{init}}^T \right)^{<2>}$

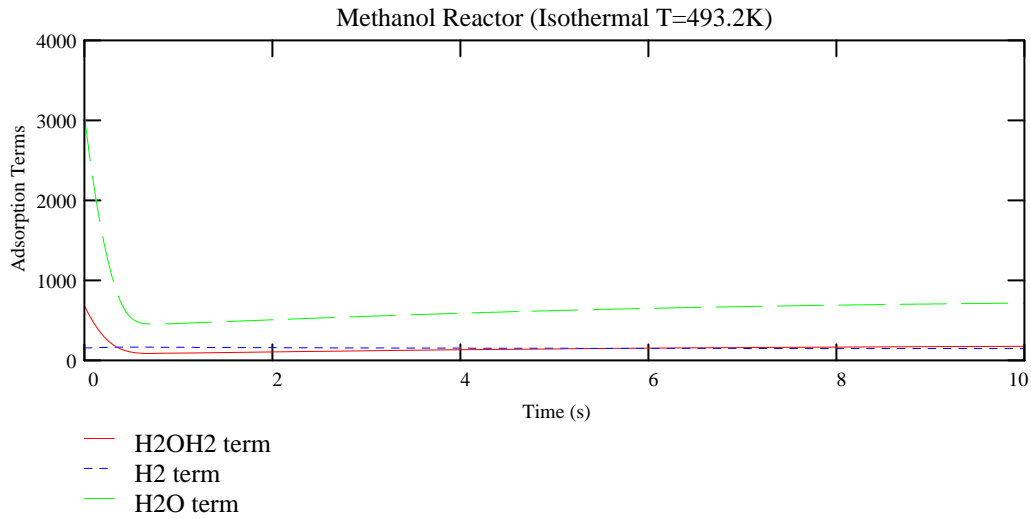
Call a routine to solve ODE in $n_{\text{step}} := 1000$ steps from $t=0$ to $t_f := 10$ sec $\text{final} := n_{\text{step}} + 1$

$$tn := \text{rkfixed}(n_{\text{init}}, 0, t_f, n_{\text{step}}, dndt) \quad t := 1 \dots \text{final} \quad \text{time} := tn^{<1>} \quad n := \text{submatrix}(tn, 1, \text{final}, 2, 9)$$

$$\Sigma n_t := \sum (n^T)^{<1>} \quad y_{t,i} := \frac{n_{t,i}}{\Sigma n_t} \quad p := y \cdot P \quad n_f := (n^T)^{<\text{final}>} \quad n_f^T = (0 \quad 0.0108 \quad 0.2096 \quad 0.021 \quad 0.1392 \quad 0 \quad 0.5 \quad 0.0398)$$



Comparison of different adsorption terms



Let us integrate without the $K_{\text{H}_2\text{OH}_2}$ term

$$r_{5.\text{approx}}(p, T) := k_{5}(T) \cdot p_{\text{CO}_2} \cdot p_{\text{H}_2} \cdot \frac{1 - \frac{1}{K_{\text{MeOH}}(T)} \cdot \frac{p_{\text{CH}_3\text{OH}} \cdot p_{\text{H}_2\text{O}}}{p_{\text{CO}_2} \cdot (p_{\text{H}_2})^3}}{\left(1 + K_{\text{H}_2}(T) \cdot \sqrt{p_{\text{H}_2}} + K_{\text{H}_2\text{O}}(T) \cdot p_{\text{H}_2\text{O}}\right)^3}$$

$$r_{2r.\text{approx}}(p, T) := k_{2r}(T) \cdot p_{\text{CO}_2} \cdot \frac{1 - \frac{1}{K_{\text{RWGS}}(T)} \cdot \frac{p_{\text{CO}} \cdot p_{\text{H}_2\text{O}}}{p_{\text{CO}_2} \cdot p_{\text{H}_2}}}{1 + K_{\text{H}_2}(T) \cdot \sqrt{p_{\text{H}_2}} + K_{\text{H}_2\text{O}}(T) \cdot p_{\text{H}_2\text{O}}}$$

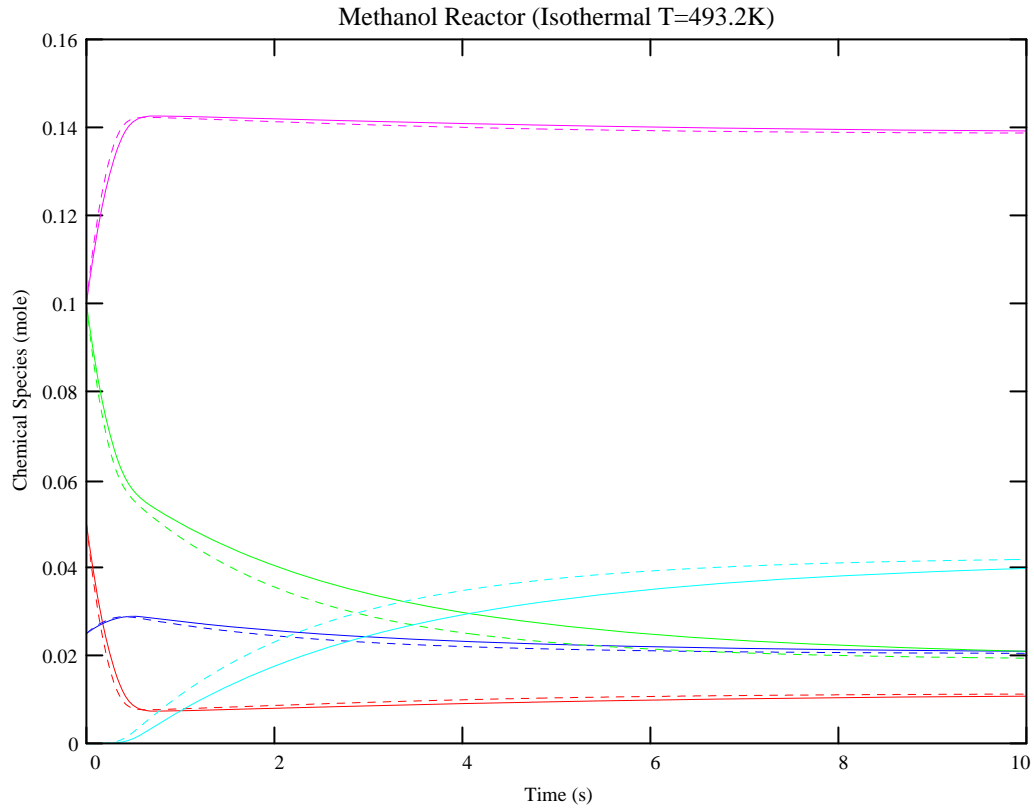
$$dndt(t, n) := m_{\text{cat}} \cdot v_5 \cdot r_{5.\text{approx}}\left(\frac{n}{\sum n}, P, T\right) + m_{\text{cat}} \cdot v_{2r} \cdot r_{2r.\text{approx}}\left(\frac{n}{\sum n}, P, T\right)$$

I.C.

$$n_{\text{init}} := \begin{pmatrix} \text{CH}_4 & \text{H}_2\text{O} & \text{H}_2 & \text{CO} & \text{CO}_2 & \text{O}_2 & \text{N}_2 & \text{CH}_3\text{OH} \\ 0 & 0.05 & 0.25 & 0.1 & 0.1 & 0 & 0.5 & 0 \end{pmatrix} \quad n_{\text{init}} := \begin{pmatrix} n_{\text{init}} \\ T \end{pmatrix}^{<2>}$$

Call a routine to solve ODE in $n_{\text{step}} := 1000$ steps from $t=0$ to $t_f := 10$ sec final := nstep + 1

$$tn := \text{rkfixed}(n_{\text{init}}, 0, t_f, n_{\text{step}}, dndt) \quad t := 1 \dots \text{final} \quad \text{time} := tn^{<1>} \quad n_{\text{approx}} := \text{submatrix}(tn, 1, \text{final}, 2, 9)$$



- H2O
- - H2O approx
- H2*0.1
- - H2*0.1 approx
- CO
- - CO approx
- CO2
- - CO2 approx
- CH3OH
- - CH3OH approx

$$n_{\text{approx.f}} := \left(n_{\text{approx}} \right)^{T^{\langle \text{final} \rangle}}$$

$$n_{\text{approx.f}} = \begin{bmatrix} 0.0000 \\ 0.0113 \\ 0.2050 \\ 0.0194 \\ 0.1387 \\ 0.0000 \\ 0.5000 \\ 0.0418 \end{bmatrix}$$

Kinetic model parameters #3 for Cu/ZnO/Al₂O₃ catalyst, from Lu, Teng, Xiao, Chemical Engineering Science, 59, 5455-5464, 2004. Eqns 8-19.

$$k_5(T) := 35.45 \cdot \exp\left(-\frac{17069}{R \cdot T}\right) \quad \text{mol/s/g catalyst, pressure in bar, } K_1 \text{ in Lu et al..}$$

$$k_2(T) := 7.3976 \cdot \exp\left(-\frac{20436}{R \cdot T}\right) \quad \text{mol/s/g catalyst, pressure in bar, } K_3 \text{ in Lu et al..}$$

$$K_{H_2}(T) := 0.249 \cdot \exp\left(\frac{34394}{R \cdot T}\right)$$

$$K_{CO_2}(T) := 1.02 \cdot 10^{-7} \cdot \exp\left(\frac{67400}{R \cdot T}\right)$$

$$K_{CO}(T) := 7.99 \cdot 10^{-7} \cdot \exp\left(\frac{58100}{R \cdot T}\right)$$

$$K_{MeOH}(T) := \exp\left(\frac{4213}{T} - 5.752 \cdot \ln(T) - 1.707 \cdot 10^{-3} \cdot T + 2.682 \cdot 10^{-6} \cdot T^2 - 7.232 \cdot 10^{-10} \cdot T^3 + 17.6\right) \dots K_{P1} \text{ in Lu et al.}$$

$$K_{WGS}(T) := 10^{\frac{2167}{T} - 0.5194 \cdot \log(T) + 1.037 \cdot 10^{-3} \cdot T - 2.331 \cdot 10^{-7} \cdot T^2 - 1.2777} \dots K_{P3} \text{ in Lu et al.}$$

$$K_{WGS}(T) := \exp\left[\ln(10) \cdot \left(\frac{2167}{T} - 0.5194 \cdot \log(T) + 1.037 \cdot 10^{-3} \cdot T - 2.331 \cdot 10^{-7} \cdot T^2 - 1.2777\right)\right]$$

methanol synthesis (Reaction 5)

$$r_5(p, T) := k_5(T) \cdot \frac{P_{CO_2} \cdot P_{H_2} \cdot \left[1 - \frac{1}{K_{MeOH}(T)} \cdot \frac{P_{CH_3OH} \cdot P_{H_2O}}{P_{CO_2} \cdot (P_{H_2})^3}\right]}{\left(1 + K_{CO_2}(T) \cdot P_{CO_2} + K_{CO}(T) \cdot P_{CO} + \sqrt{K_{H_2}(T) \cdot P_{H_2}}\right)^3}$$

forward WGS (Reaction 2)

$$r_2(p, T) := k_2(T) \cdot \frac{P_{H_2O} - \frac{1}{K_{WGS}(T)} \cdot \frac{P_{CO_2} \cdot P_{H_2}}{P_{CO}}}{1 + K_{CO_2}(T) \cdot P_{CO_2} + K_{CO}(T) \cdot P_{CO} + \sqrt{K_{H_2}(T) \cdot P_{H_2}}}$$

Isothermal Methanol Reactor. $T := 500 \text{ K}$ $P := 100 \text{ bar}$

$m_{cat} := 1640 \text{ g catalyst}$; this roughly corresponds to an initial void fraction of $a=0.5$ and catalyst density of $\rho=2000 \text{ kg/m}^3$ at $T=500 \text{ K}$ & $P=50 \text{ bar}$ (numbers chosen for easy calculation; may be a what-if)

$$V := \frac{R \cdot T}{50 \cdot 10^5} \quad V = 8.314 \cdot 10^{-4} \text{ m}^3/\text{mole reactant} \quad 2000 \cdot V = 1.663 \text{ kg/mole reactant}$$

$$dndt = v \cdot r = v_5 \cdot r_5 + v_2 \cdot r_2 \quad v_2 := -v_2 r$$

$$dndt(t, n) := m_{cat} \cdot v_5 \cdot r_5\left(\frac{n}{\sum n}, P, T\right) + m_{cat} \cdot v_2 \cdot r_2\left(\frac{n}{\sum n}, P, T\right)$$

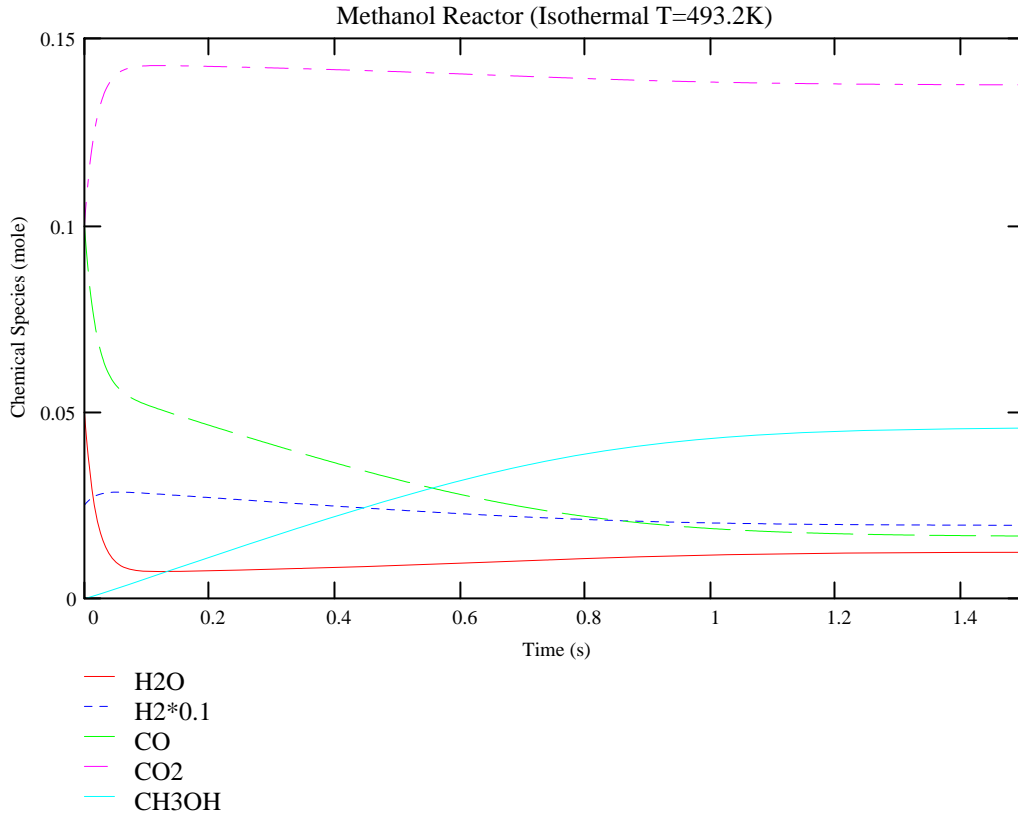
I.C.

$$n_{\text{init}} := \begin{pmatrix} \text{CH4} & \text{H2O} & \text{H2} & \text{CO} & \text{CO2} & \text{O2} & \text{N2} & \text{CH3OH} \\ 0 & 0.05 & 0.25 & 0.1 & 0.1 & 0 & 0.5 & 0 \end{pmatrix} \quad n_{\text{init}} := \begin{pmatrix} n_{\text{init}} \\ T \end{pmatrix}^{<2>}$$

Call a routine to solve ODE in nstep := 1000 steps from t=0 to t_f := 1.5 final := nstep + 1

$$tn := \text{rkfixed}(n_{\text{init}}, 0, t_f, nstep, dndt) \quad t := 1 \dots \text{final} \quad \text{time} := tn^{<1>} \quad n := \text{submatrix}(tn, 1, \text{final}, 2, 9)$$

$$\Sigma n_t := \sum (n T)^{<t>} \quad y_{t,i} := \frac{n_{t,i}}{\Sigma n_t} \quad p := y \cdot P \quad n_f := (n T)^{<\text{final}>} \quad n_f T = (0 \quad 0.0124 \quad 0.1963 \quad 0.0168 \quad 0.1376 \quad 0 \quad 0.5 \quad 0.0456)$$

Let us approximate the K_{MeOH} & K_{WGS} terms

$$K_{\text{MeOH}}(T) := \exp\left(\frac{4213}{T} - 18.043\right)$$

$$K_{\text{WGS}}(T) := \exp\left[\ln(10) \cdot \left(\frac{2167}{T} - 2.212\right)\right]$$

methanol synthesis (Reaction 5)

$$r_{5,\text{approx}}(p, T) := k_5(T) \cdot \frac{p_{\text{CO2}} \cdot p_{\text{H2}} \cdot \left[1 - \frac{1}{K_{\text{MeOH}}(T)} \cdot \frac{p_{\text{CH3OH}} \cdot p_{\text{H2O}}}{p_{\text{CO2}} \cdot (p_{\text{H2}})^3}\right]}{\left(1 + K_{\text{CO2}}(T) \cdot p_{\text{CO2}} + K_{\text{CO}}(T) \cdot p_{\text{CO}} + \sqrt{K_{\text{H2}}(T) \cdot p_{\text{H2}}}\right)^3}$$

forward WGS (Reaction 2)

$$r_{2, \text{approx}}(p, T) := k_2(T) \cdot \frac{P_{\text{H}_2\text{O}} - \frac{1}{K_{\text{WGS}}(T)} \cdot \frac{P_{\text{CO}_2} \cdot P_{\text{H}_2}}{P_{\text{CO}}}}{1 + K_{\text{CO}_2}(T) \cdot P_{\text{CO}_2} + K_{\text{CO}}(T) \cdot P_{\text{CO}} + \sqrt{K_{\text{H}_2}(T) \cdot P_{\text{H}_2}}}$$

$$\text{dndt}(t, n) := m_{\text{cat}} \cdot v_5 \cdot r_{5, \text{approx}}\left(\frac{n}{\sum n}, P, T\right) + m_{\text{cat}} \cdot v_2 \cdot r_{2, \text{approx}}\left(\frac{n}{\sum n}, P, T\right)$$

I.C. $n_{\text{init}} := \begin{pmatrix} \text{CH}_4 & \text{H}_2\text{O} & \text{H}_2 & \text{CO} & \text{CO}_2 & \text{O}_2 & \text{N}_2 & \text{CH}_3\text{OH} \\ 0 & 0.05 & 0.25 & 0.1 & 0.1 & 0 & 0.5 & 0 \end{pmatrix}$ $n_{\text{init}} := \begin{pmatrix} n_{\text{init}} \\ T \end{pmatrix}^{<2>}$

Call a routine to solve ODE in nstep := 1000 steps from t=0 to t_f := 1.5 sec final := nstep + 1

$$\text{tn} := \text{rkfixed}(n_{\text{init}}, 0, t_f, \text{nstep}, \text{dndt}) \quad t := 1 \dots \text{final} \quad \text{time} := \text{tn}^{<1>} \quad n_{\text{approx}} := \text{submatrix}(\text{tn}, 1, \text{final}, 2, 9)$$

